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The very first question is what  
problem are we trying to solve?

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Is it local air quality?

or

Is it impact on Global Warming?

or

Is it best economic performance?

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CO<sub>2</sub> is such a great concern because  
it accumulates in the atmosphere

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# What is aviation's absolute contribution to the CO<sub>2</sub> problem?

- How much air is there in the atmosphere?
  - About 5200 tera tonnes ( $5.2 \times 10^{15}$  tonnes)
- How much CO<sub>2</sub> is there in the atmosphere today?
  - About 3 tera tonnes
- How much extra will aviation add this year?
  - About 0.0007 tera tonnes
  - An increase of 0.023%

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# The CO<sub>2</sub> lake

- In every cubic metre of this room, there are 1 million ccs of air.
- In every cubic metre of this room, there are about 375 ccs of CO<sub>2</sub>
- This is equivalent to a pint glass 2/3 full for each cubic metre

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# How quickly is the lake growing?

- This year aviation will consume about 220 million tonnes of kerosene
- The (optimistic) forecast for future growth in air transport capacity is 5% per year
- Fuel burn per aircraft decreases at about 1.5% per year as new technology aircraft enter the global fleet
- Total fuel burn could grow at 3.5% per year

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# Is the world being driven to destruction by evil aviation?

- By 2050 the annual fuel burn could be 1 billion tonnes of kerosene
- The amount of aviation generated CO<sub>2</sub> in 2050 could be 3 billion tonnes
- The total amount of CO<sub>2</sub> added to the lake between 2008 and 2050 could be as much as 68 billion tonnes

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# Therefore

- By 2050, this would be an increase of 2.4% in the size of the “CO<sub>2</sub> lake”
- At these rates, it would take aviation 1000 years of operation before the pint glass was full



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# What determines the fuel burn?

- During the flight the engines burn fuel and the total mass of the aircraft decreases

$$\dot{M} = -\dot{m}f$$

- Also in the cruise –

$$T = D \qquad Mg = L$$

- Now the overall efficiency  $\eta_0$  is given by

$$\eta_0 = \frac{(D \times V_\infty)}{(\dot{m}f \times LCV)}$$

- Where LCV is the lower calorific value for the fuel

- Now if the aircraft is flying at constant Mach number and at a fixed value fraction of the maximum lift to drag ratio (constant n)

$$-\dot{M} = \frac{(Mg \times V_\infty)}{\left( LCV \times n \times \left( \eta_0 \times \left( \frac{L}{D} \right)_{\max} \right) \right)}$$

but  $V_\infty = \frac{dS}{dt}$  where S is the distance flown

$$-\frac{dM}{M} = \frac{g}{n \times \left( \eta_0 \times \left( \frac{L}{D} \right)_{\max} \right) \times LCV} \cdot dS$$

- Therefore, if the total distance flown is R the fuel used is

$$\frac{(MF)_{cruise}}{MTO} = 1 - EXP \left[ - \frac{(g \times R / LCV)}{\left( \eta_0 \times n \times \left( \frac{L}{D} \right)_m \right)} \right]$$

- For simplicity let

$$X = \frac{g \times R}{LCV \times n \times \left( \eta_0 \times \left( \frac{L}{D} \right) \right)_{\max}}$$

- And, if the additional fuel used for climb is

$$\frac{\Delta mf_{climb}}{M_{TO}} = 1 - k$$

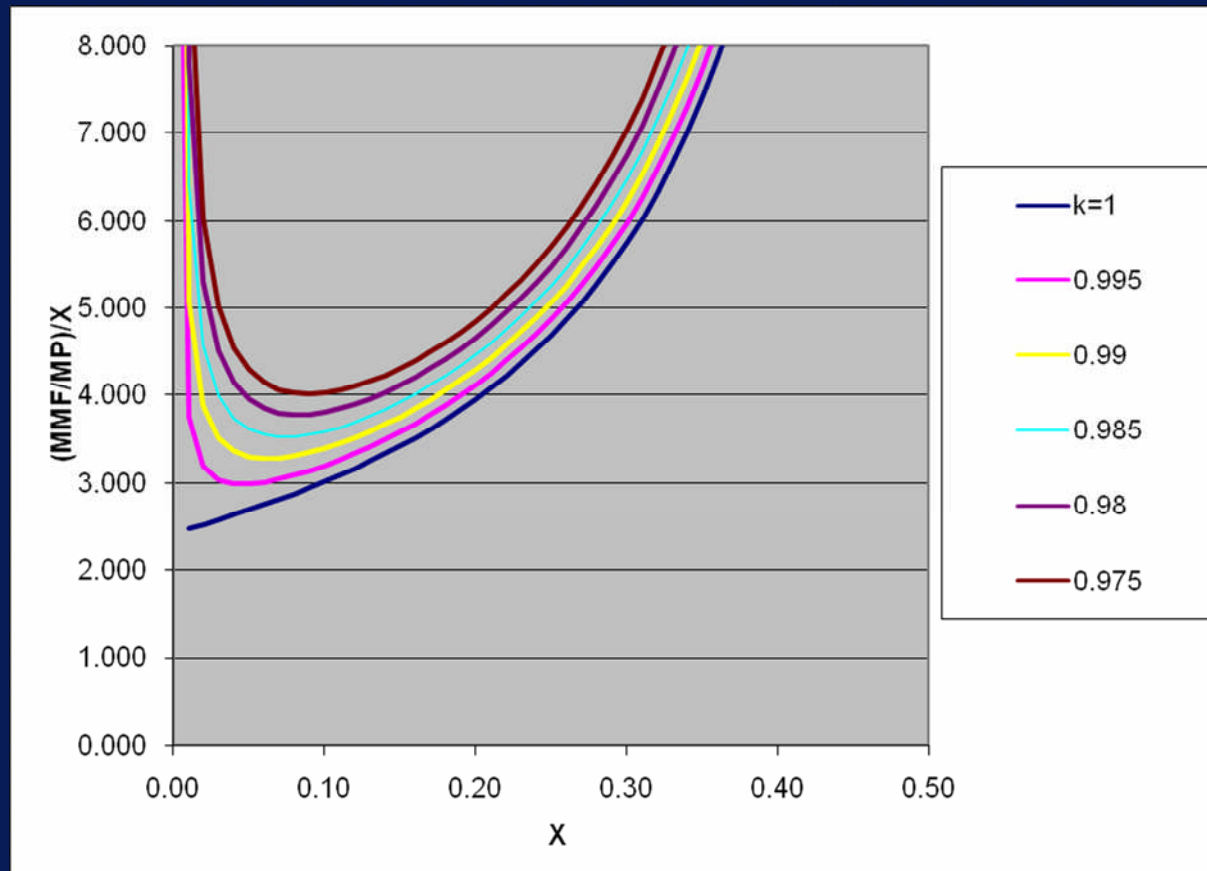
- Then

$$\frac{MMF}{MTO} = 1 - k \text{EXP}(-X)$$

- However, the usual economic parameter is

$$\frac{MMF}{(MP \times X)}$$

# Sensitivity of $MMF/(MP \cdot X)$ to $k$



# Sensitivity of $MMF/(MP \cdot X)$ to $MOE/MMTO$

