

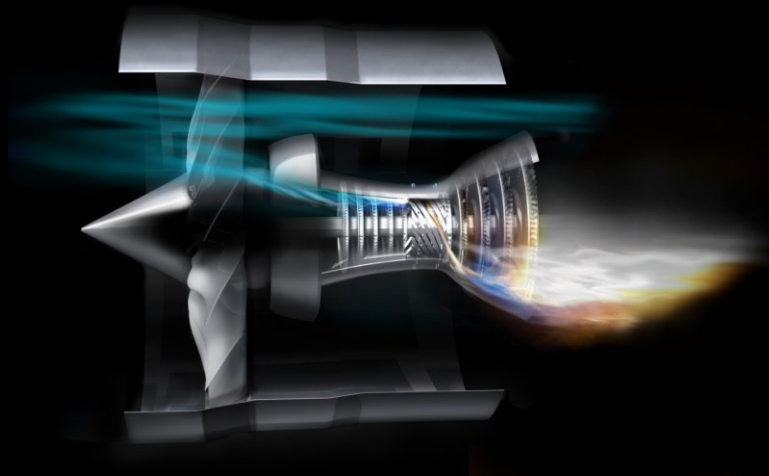


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Progress in heat management for hydrogen combustion aircraft

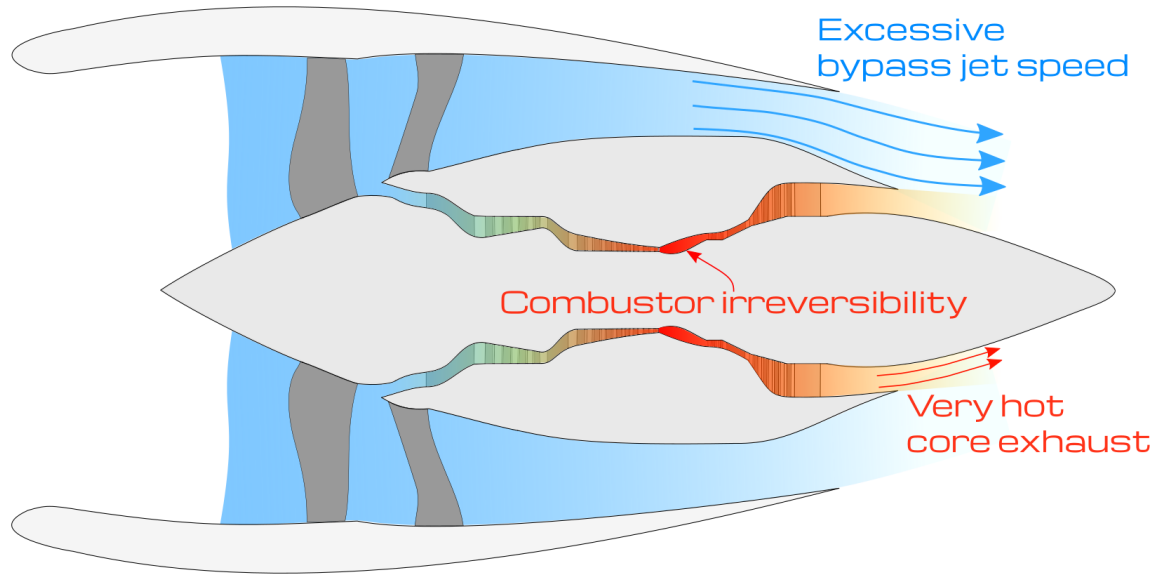
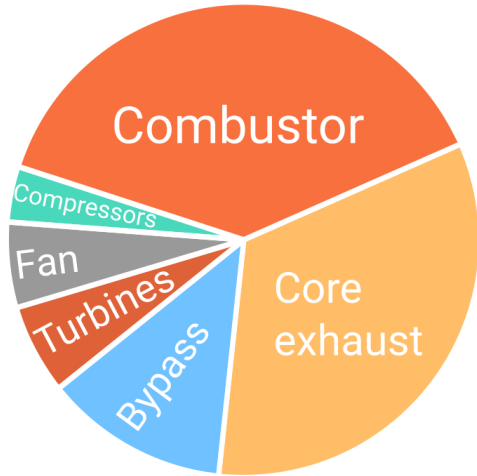
Tomas Grönstedt, professor turbomachinery
Chalmers University, Sweden
tomas.gronstedt@chalmers.se

Major contributions also by: Carlos Xisto,
Isak Jonsson, Alexandre Capitao-Patrao



ULTIMATE (EU project - 2015 – 2018)

Ultra Low emission Technology Innovations for Mid-century Aircraft Turbine Engines

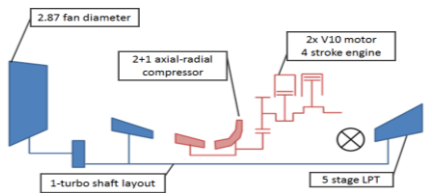
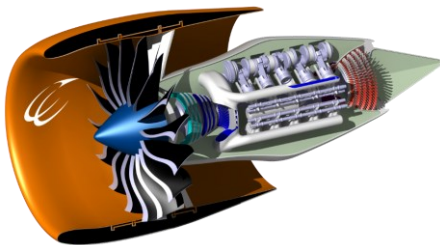


Grönstedt, Tomas, Carlos Xisto, Vishal Sethi, Andrew Rolt, Nicolás García Rosa, Arne Seitz, Kyros Yakinthos et al. "Ultra low emission technology innovations for mid-century aircraft turbine engines." *Turbo Expo: Power for Land, Sea, and Air*, vol. 49743, p. V003T06A001. American Society of Mechanical Engineers, 2016.

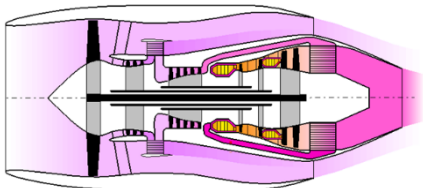
Efficiency improvement potential

CO₂ reduction relative to year 2000

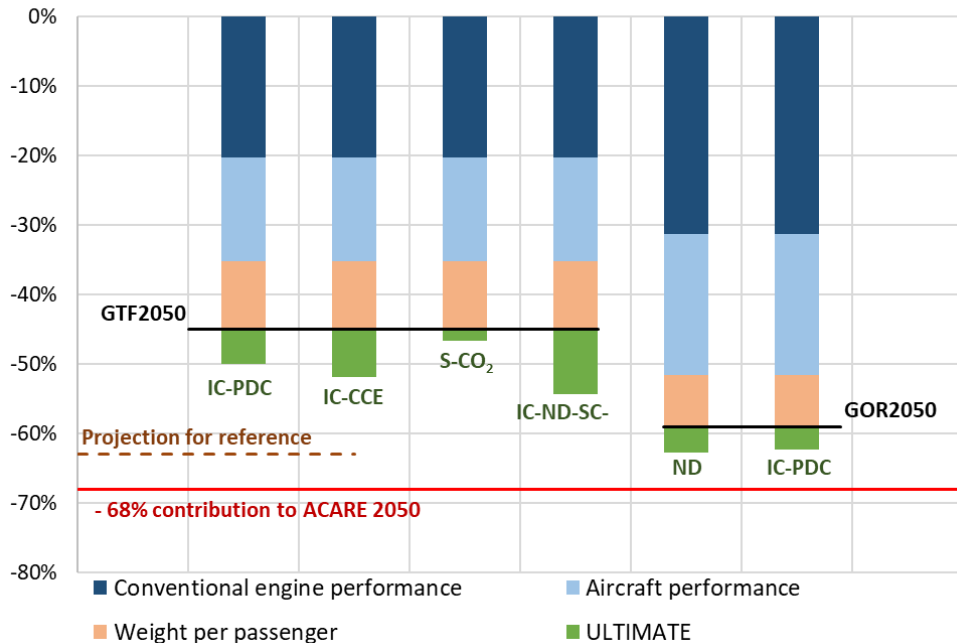
Pressure gain combustion



Core exhaust heat recovery



Grönstedt, Tomas, Carlos Xisto, Vishal Sethi, Andrew Rolt, N. G. Roas, Arne Seitz, D. Misirliis, John Whurr, Nicolas Tantot, and Martin Dietz. "Conceptual design of ultra-efficient cores for mid-century aircraft turbine engines." In *Proceedings of the 24th ISABE Conference, Canberra, Australia*, pp. 22-27. 2019.



Ultra low specific thrust

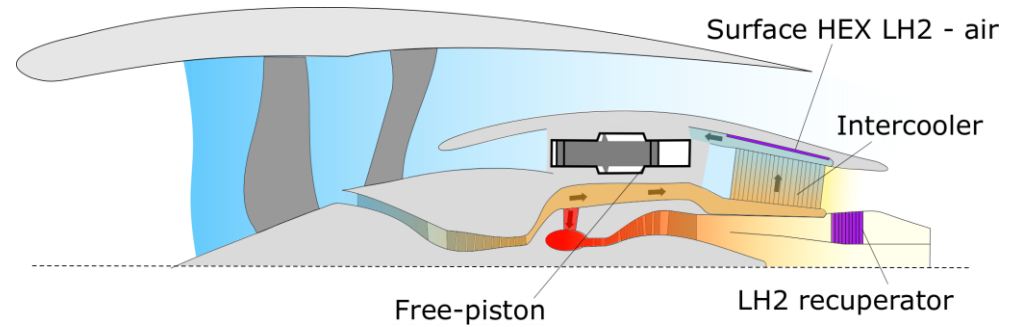
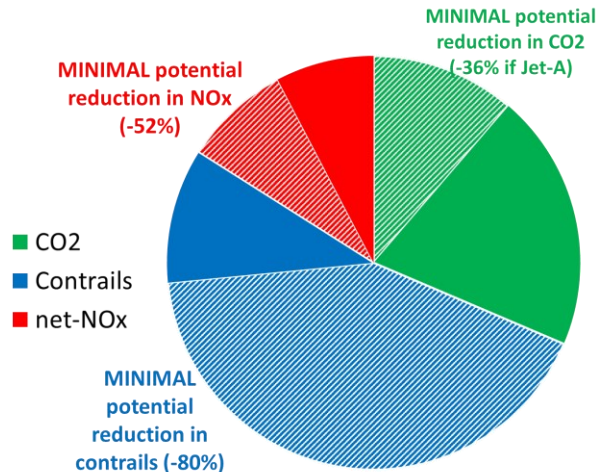
Boxprop



MINIMAL (2022-2026)



- Step improvement in thermal efficiency.
- Operational flexibility
- Heavy-duty proven NOx mitigation technology
- Attack in all fronts



REACTION ENGINES



Rolls-Royce



Delft University of Technology



Bauhaus Luftfahrt
Neue Wege.

ARISTOTLE
UNIVERSITY OF
THESSALONIKI

Climate impact of targets

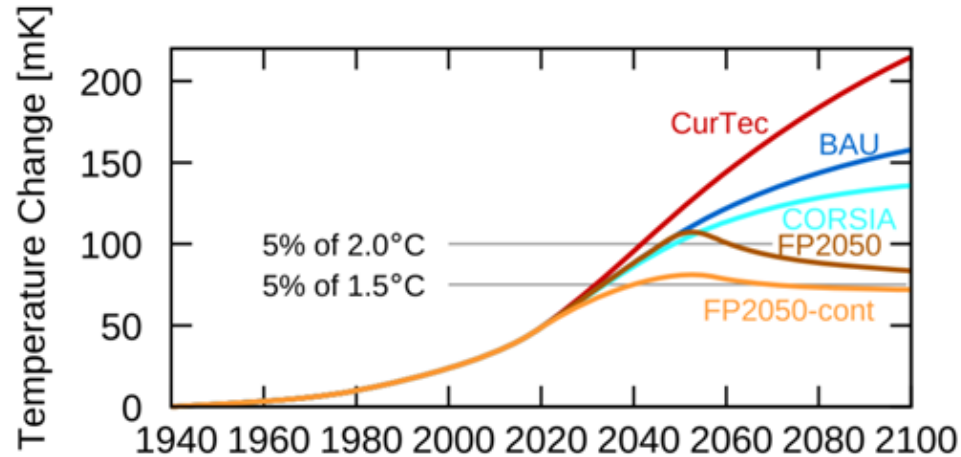
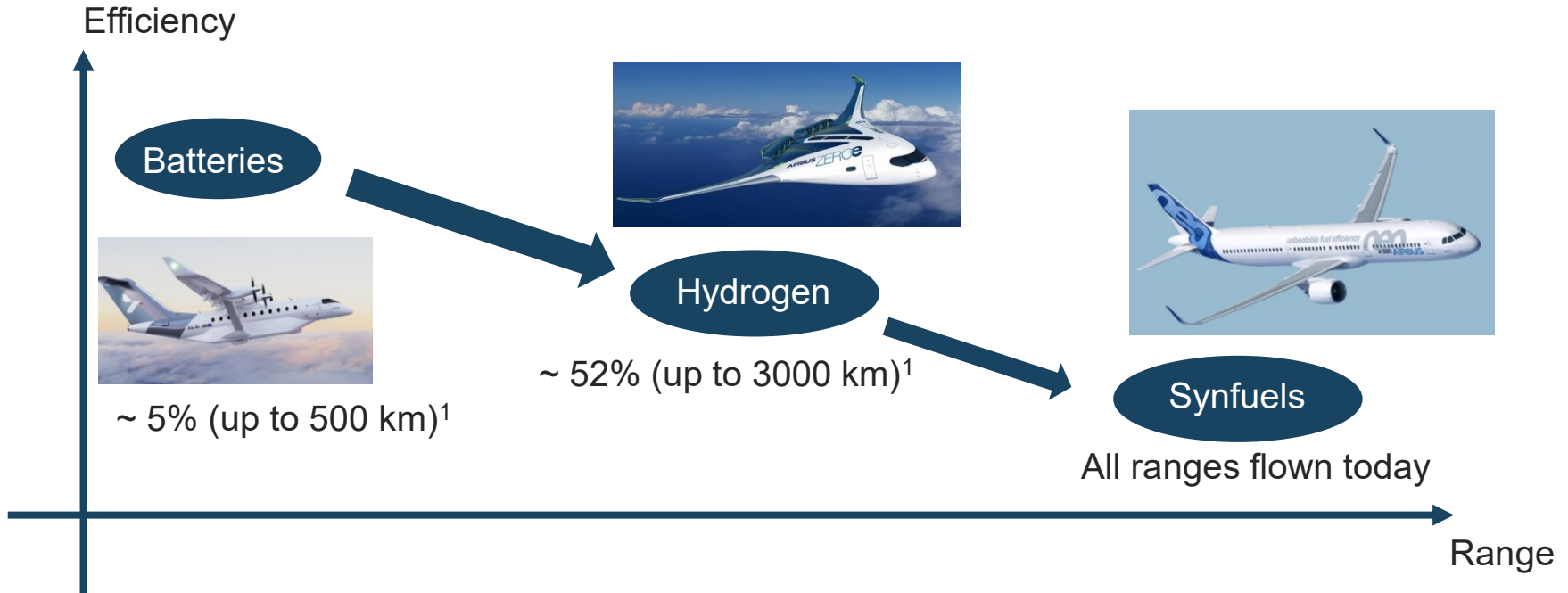


Fig. 2 Near-surface temperature change of five scenarios including CO₂ and non-CO₂-effects.

Grewe, V., Gangoli Rao, A., Grönstedt, T. *et al.* Evaluating the climate impact of aviation emission scenarios towards the Paris agreement including COVID-19 effects. *Nat Commun* **12**, 3841 (2021).
<https://doi.org/10.1038/s41467-021-24091-y>

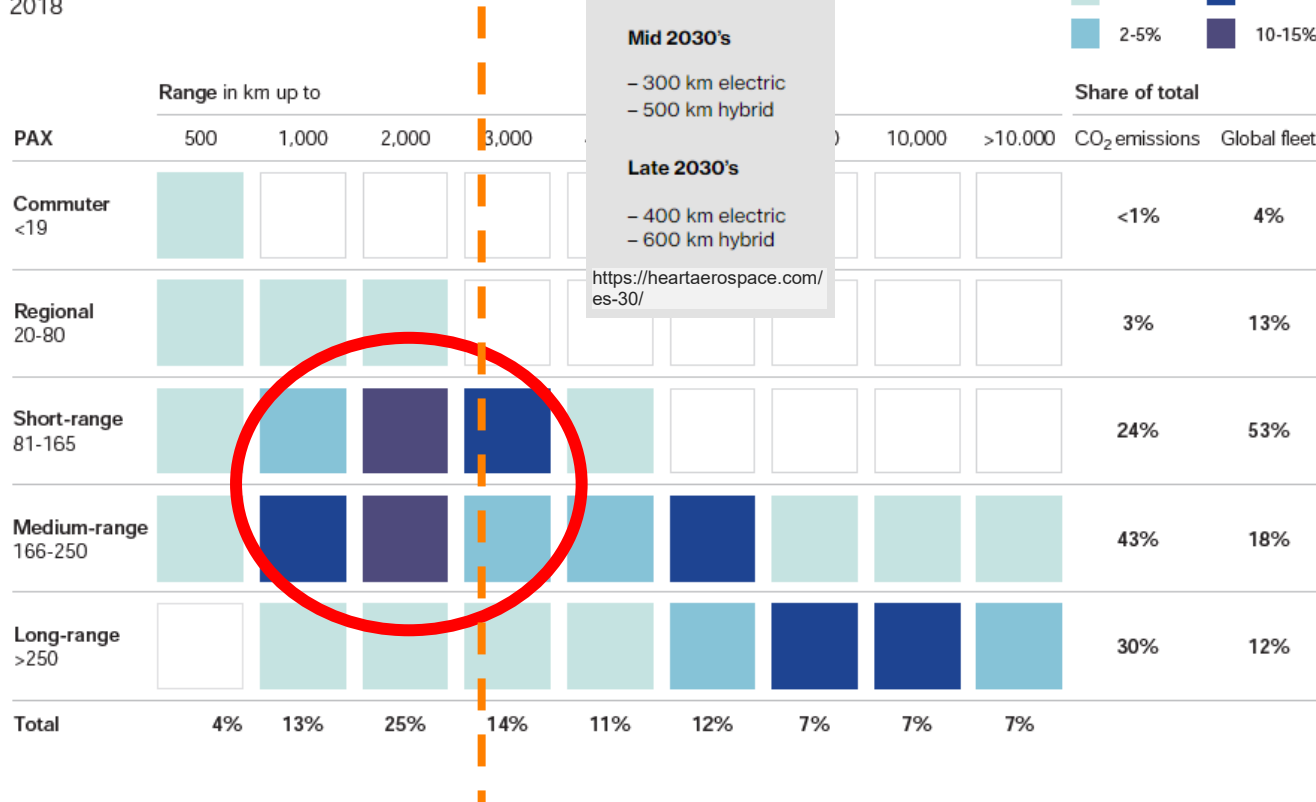
Impact vs efficiency of hydrogen



¹Graver, Brandon, Kevin Zhang, and Dan Rutherford. "emissions from commercial aviation, 2018." ICCT, 2019.

CO₂ emissions per segment and range

2018



Late 2020's
 - 200 km electric
 - 400 km hybrid

Mid 2030's
 - 300 km electric
 - 500 km hybrid

Late 2030's
 - 400 km electric
 - 600 km hybrid

<https://heartaerospace.com/es-30/>

□ Negligible contribution

0-2% 5-10%
 2-5% 10-15%

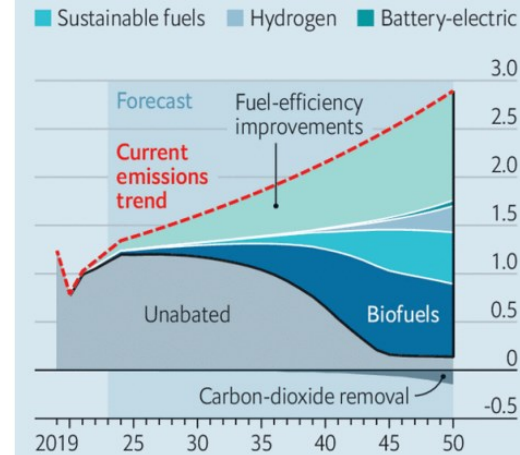
Share of total
 CO₂ emissions Global fleet



Operating beyond distances of 2,222 km in a single-stage flight would require a battery pack specific energy of at least 1,600 Wh/kg

Gnadt, A. R. Technical and Environmental Assessment of All-Electric 180-Passenger Commercial Aircraft. SM thesis, MIT, 2018

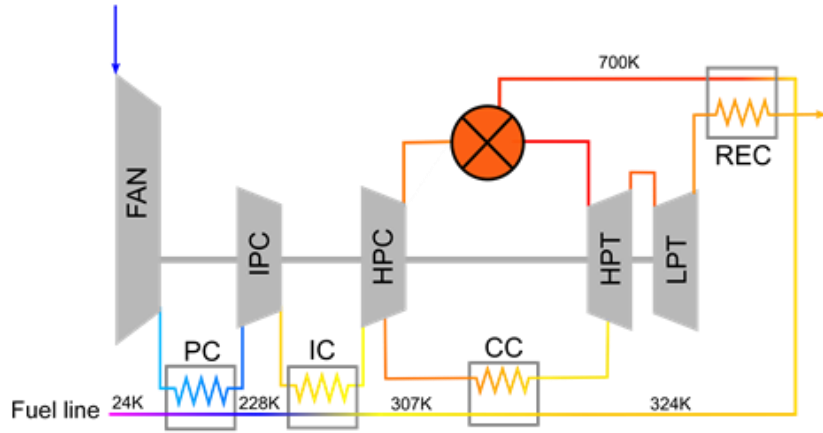
The economist, 30 May, 2023



Hydrogen-powered aviation
 A fact-based study of hydrogen technology, economics, and climate impact by 2050

Heat management

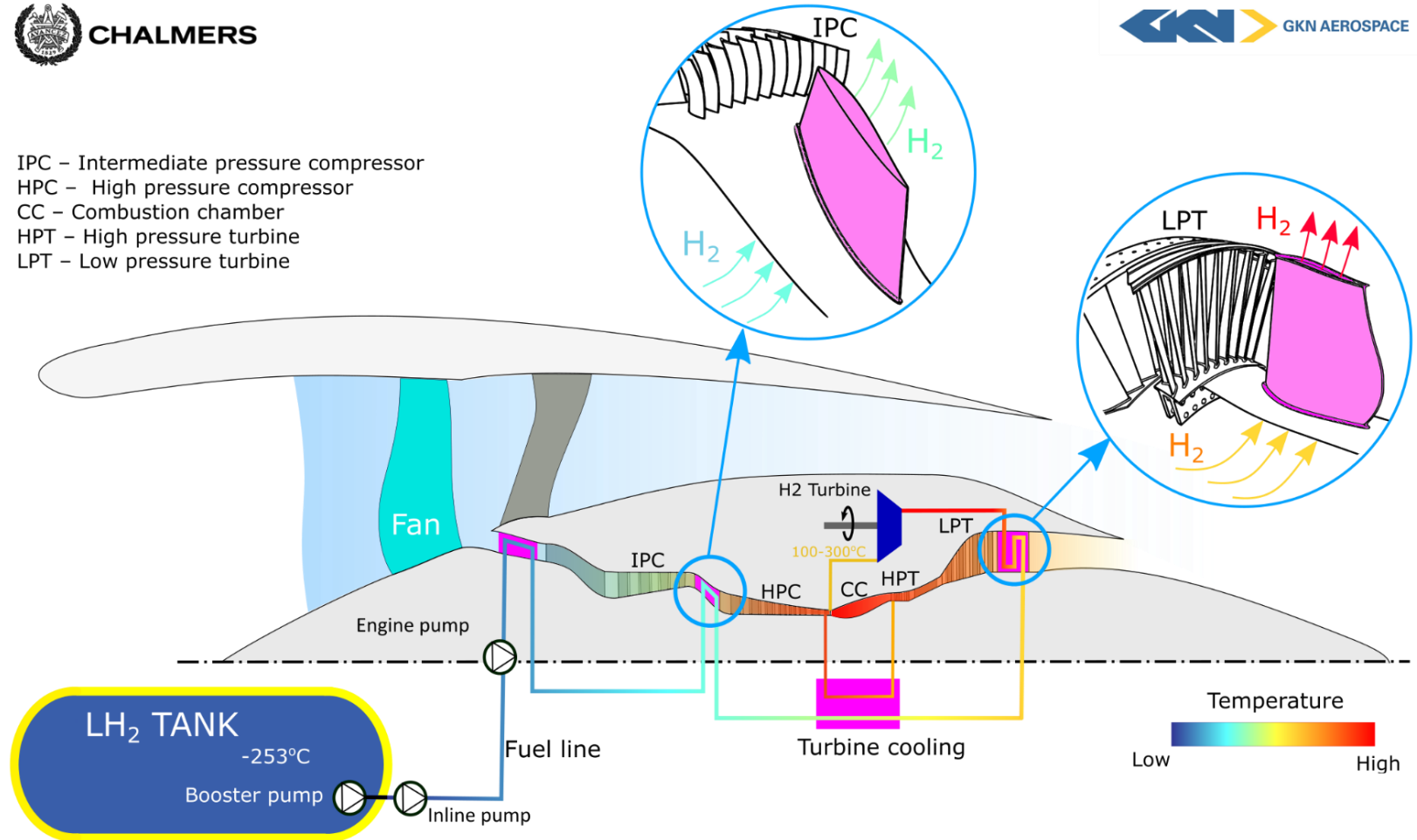
Cryogenic hydrogen Heat management research



Temperature	Pressure	Enthalpy
22 K	2.3 bar	17.84 kJ/kg
700 K	40 bar	9793.5 kJ/kg
1000 K	40 bar	14229 kJ/kg

- Heat addition to fuel could easily be 10% of fuel heat value
 - theoretically ~ 10% SFC!
- Advanced engine integration may allow further improvement

IPC – Intermediate pressure compressor
 HPC – High pressure compressor
 CC – Combustion chamber
 HPT – High pressure turbine
 LPT – Low pressure turbine

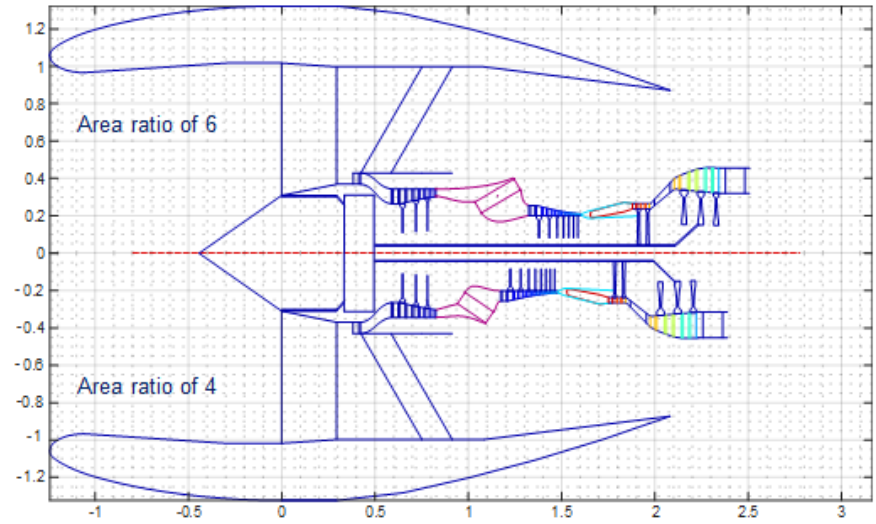
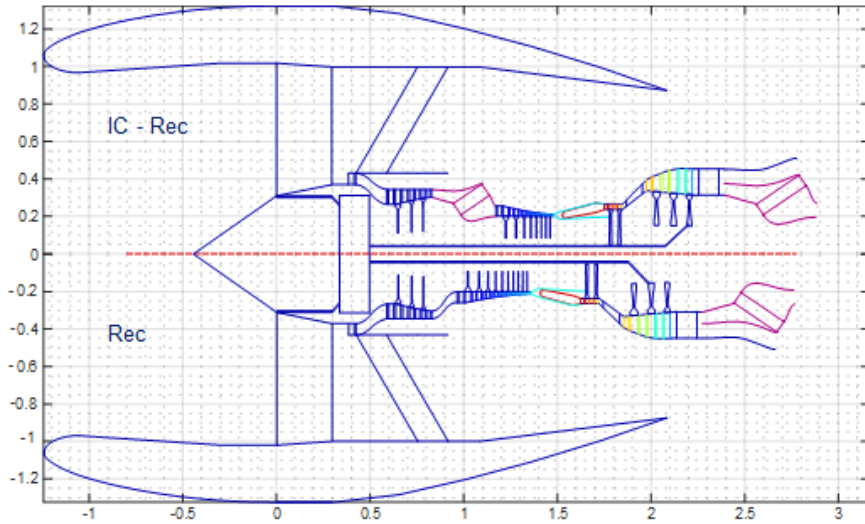


Propulsion system integration (IPC/LPT)



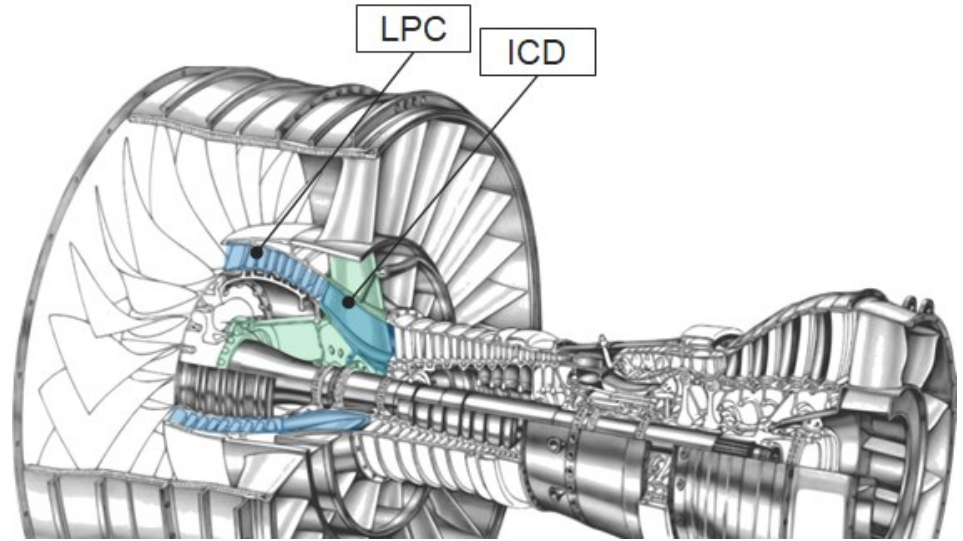
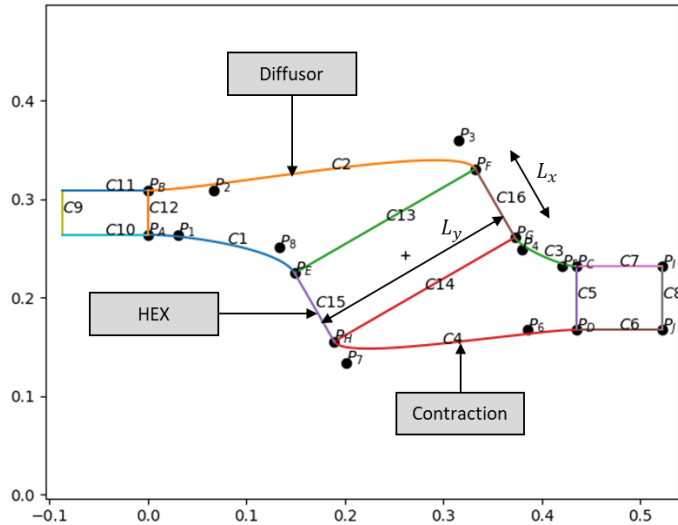
ENABLE H2

AR4/AR6 – area ratio
of diffuser

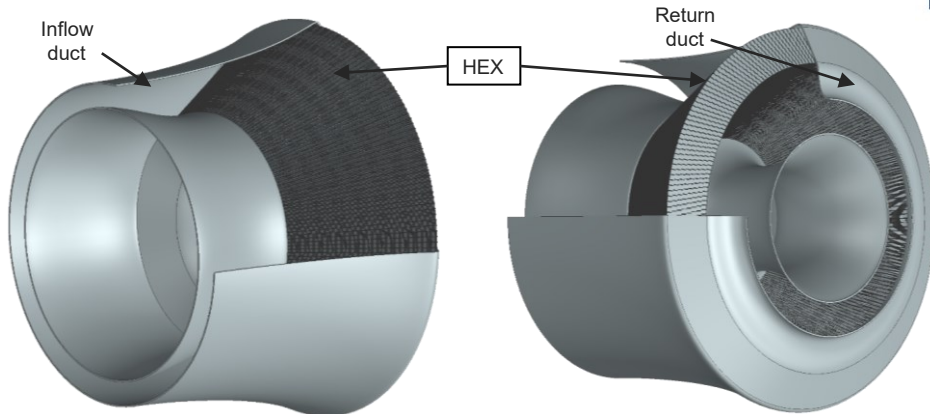


Hydrogen heat recovery system – compression side (IPC)

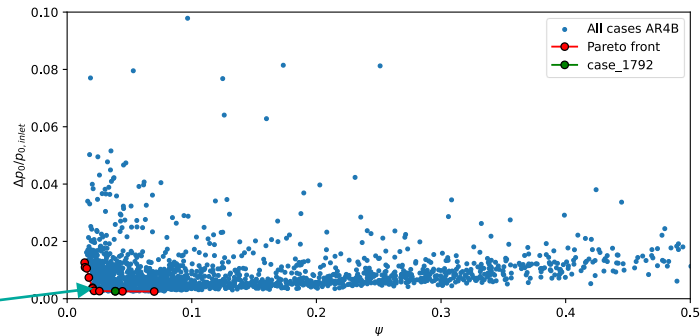
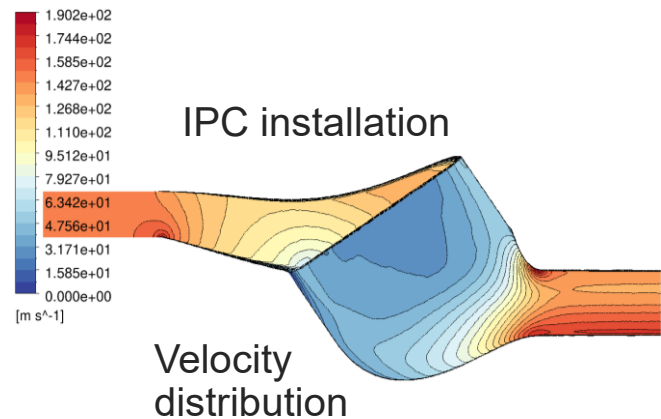
- Finned tube design
- Optimization of diffuser and contraction ducts
- 19 design parameters



IPC installation



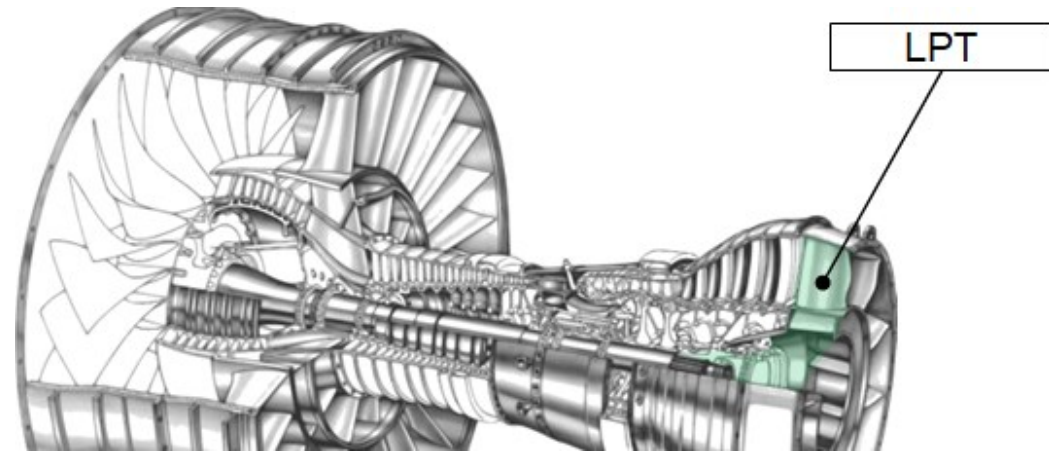
- Achieve low pressure loss and good flow uniformity



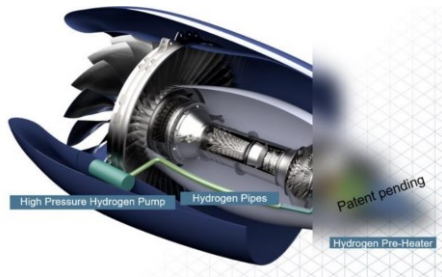
$$\psi = \frac{\int_{A_{inlet}} \frac{1}{2} v'^2 dA}{\int_{A_{inlet}} \frac{1}{2} V^2 dA}$$

$$v' = V - \int_{A_{inlet}} V dA$$

LPT installation



- Work close with GKN Aerospace
- Successful testing and demonstration of new pre-heater concept



System predictions

Variant	Mass (kg)	Architecture	$\Delta_{FB,SFC}$	$\Delta_{FB,W}$	Δ_{FB} (3000 NM)
Baseline	3185	1+3+10+2+3	datum	datum	datum
Intercooled AR4	3127	1+3+8+2+3	-2.06%	-0.26%	-2.3%
Intercooled AR6	3159	1+3+7+2+3	-2.96%	-0.12%	-3.1%
Intercooler AR4 Recuperated AR4	3440	1+3+8+2+3	-5.94%	1.17%	-4.8%
Recuperated AR4	3390	1+3+10+2+3	-5.94%	0.93%	-5.1%

Low-Pressure Compressor Facility At Chalmers

2.5 Stage Compressor

1.2 m diameter, 2.5 stage low-pressure compressor provides representative operation

Wide operation Space

Reynolds numbers up to $Re_c = 600,000$

Stable Operation

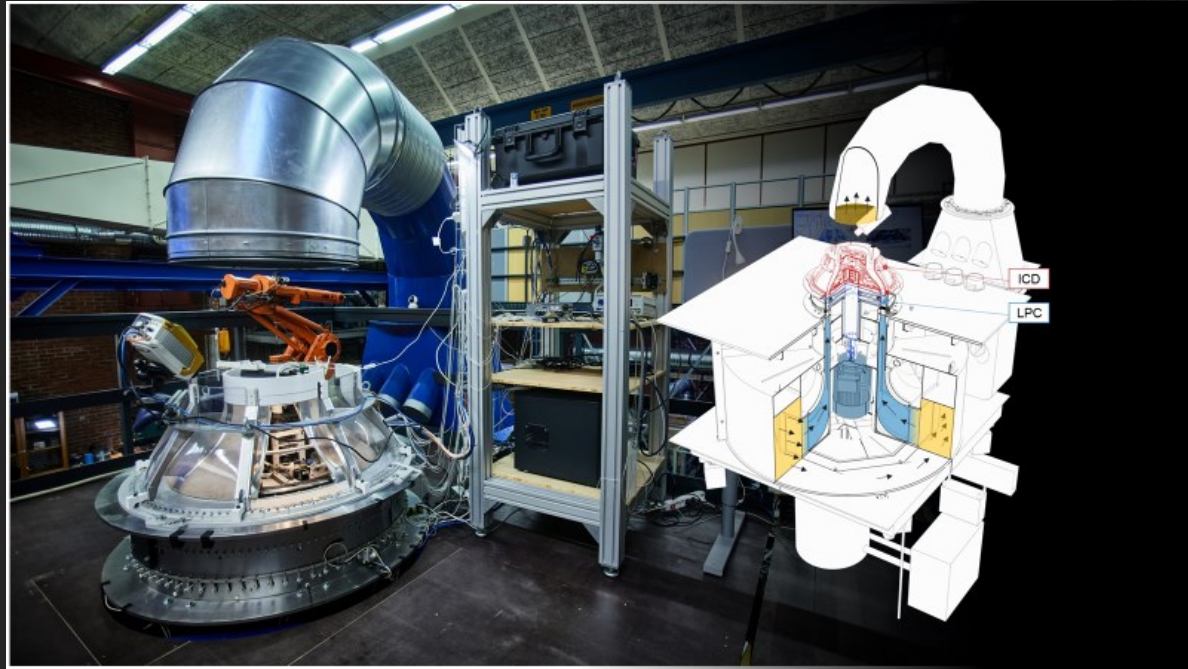
Continuous operation near stall up to 16 hour allows for detailed studies.

Aerothermal Investigation

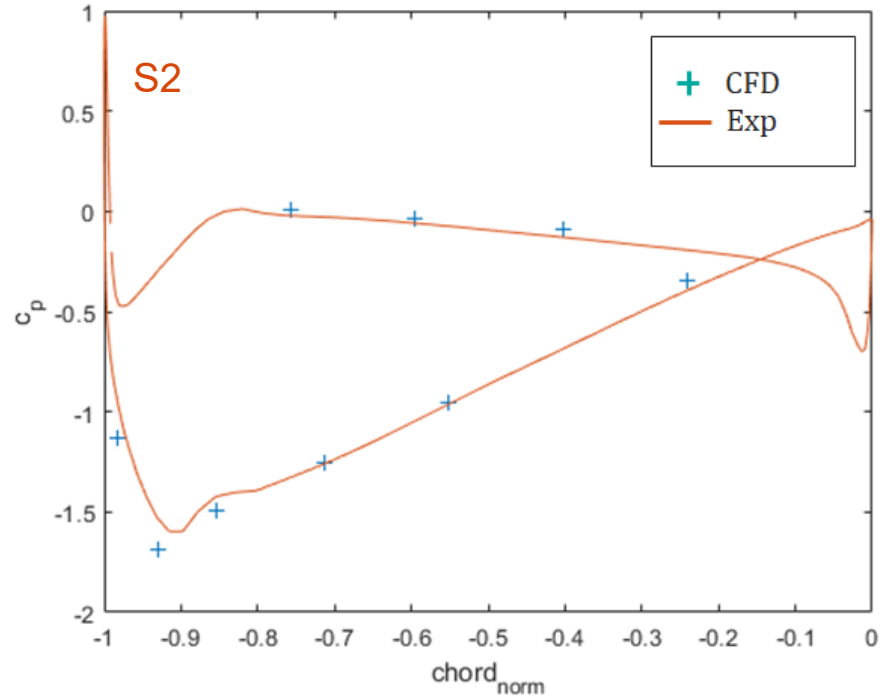
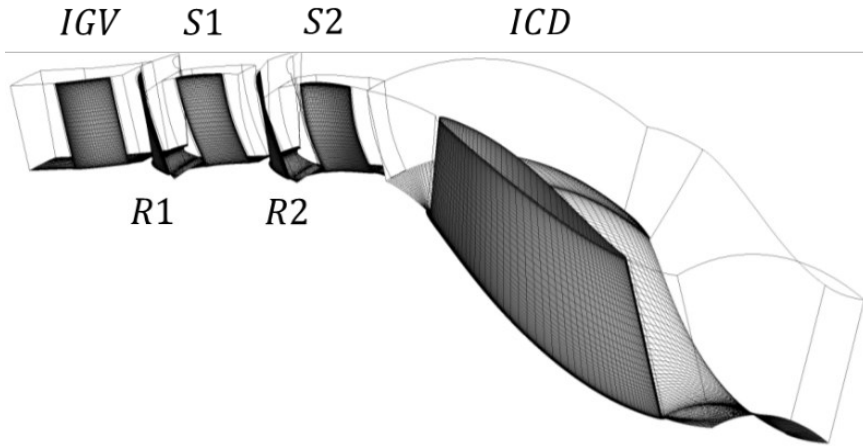
Build for advanced measurement with; several Multi-hole probes, PIV, IR-thermography, Hot-wire, Pressure taps...

Excellent Access and Modularity

Build for modularity and access and an entire ICD can be changed with less than 20 min downtime.

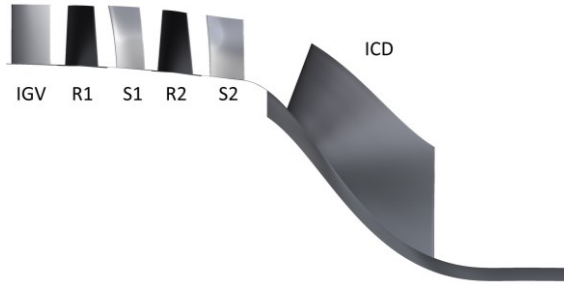


Validation with CFD



- ANSYS - CFX
- $k - \omega$ SST
- $\gamma - \theta$ transition model
- Semi-perfect gas

- 100% speed tests
- Good flow uniformity



- Heat transfer and flow uniformity validations on-going
- So far so good.
- Work on regularizing conditions, currently S2 ICD (wake transition)

ENABLEH2 Compressor

Rotational Speed	1920 rpm
Mass flow	17 kg/s
Pressure ratio	1.07
Tip Speed	100 m/s
Axial Velocity	70 m/s
Rotor Re_c	600 000
Avg Tip radius	620 mm
Avg Hub radius	540 mm
N. stator Blades (IGV, S1, OGV, ICD)	75, 126, 124, 8
N. rotor Blades (R1, R2)	61, 69
Avg Aspect Ratio	2.157
Avg Tip Clearance	0.75 mm

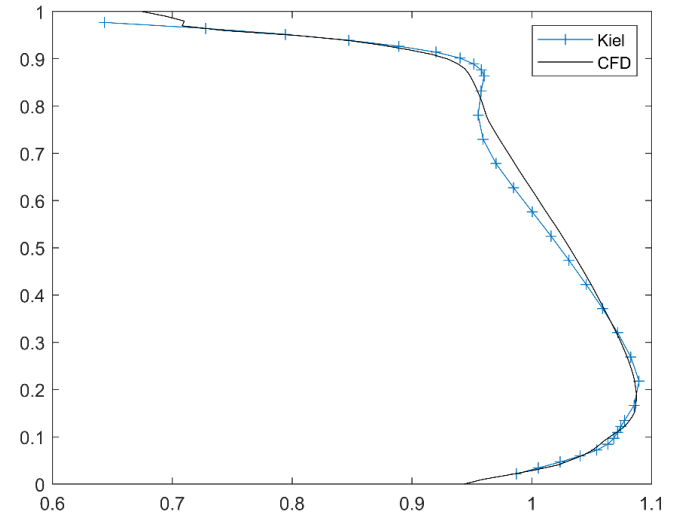


Figure 6-5 Normalised total pressure at the inlet of S2 for Kiel probe measurements and numerical simulations (sector integrated, 2000 pts in 15 deg.)



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Cryo-tanks

07:48 Voil 4G+ LTEV 30%



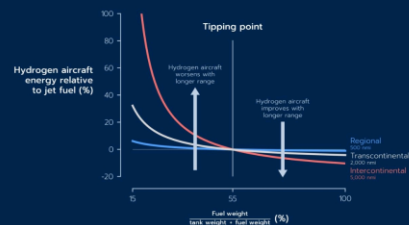
Joaquim R. R. A. M...ns (Han/honom) · Följer
Professor of Aerospace Engineering at the...
1 mån ·

Some say hydrogen-powered aircraft are only suitable for shorter flights, while others say they're better as the distance increases. This apparent contradiction stems from different assumptions on tank weight. In my review paper with [Eytan Adler](#), we show that with light enough tanks, hydrogen aircraft could use less energy than current aircraft for all flight distances.

You can read the full paper here:

<https://lnkd.in/gx7k5wkD>

#aircraft #aviation #mdolab #hydrogen #hydrogenenergy #hydrogeneconomy #aircraftdesign



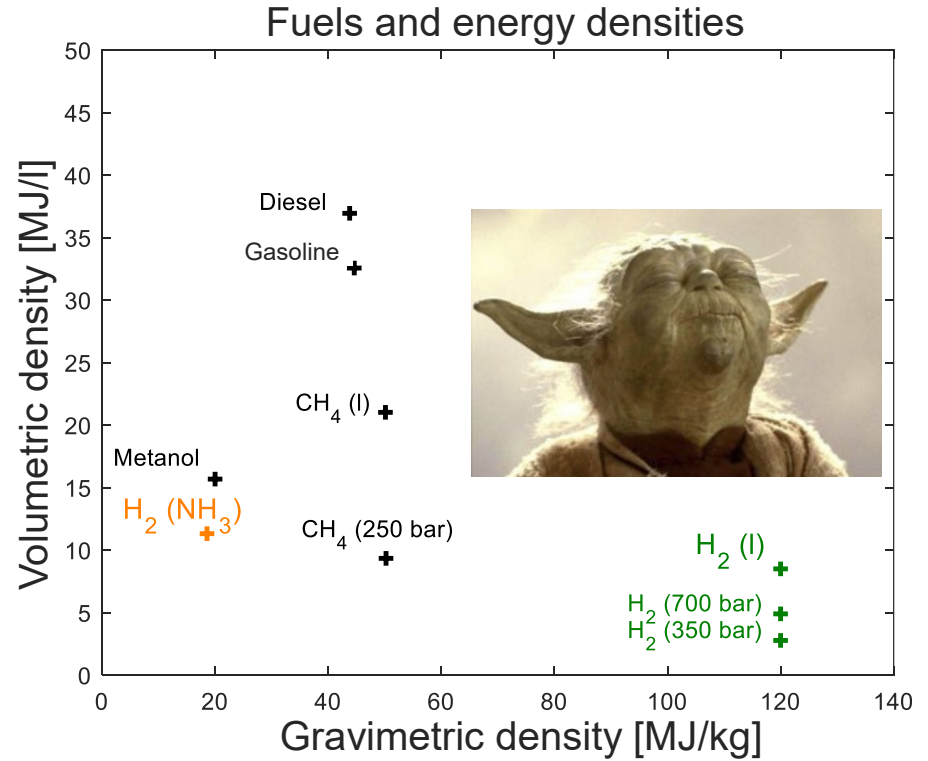
Misconception: Hydrogen aircraft actually get better at longer range - Potentially – relative to jet fuel.
(R. Miller, Cambridge, 2023-04-26, ETC conference)

Hydrogen – storage properties

$q_{grav} = \text{heat content per mass [kWh/kg]}$

$q_{vol} = \text{heat content per volume [kWh/litre]}$

- Hydrogen has extremely high energy density per kg
- But it has low energy density per volume
- Transportation in form of ammonia may be attractive

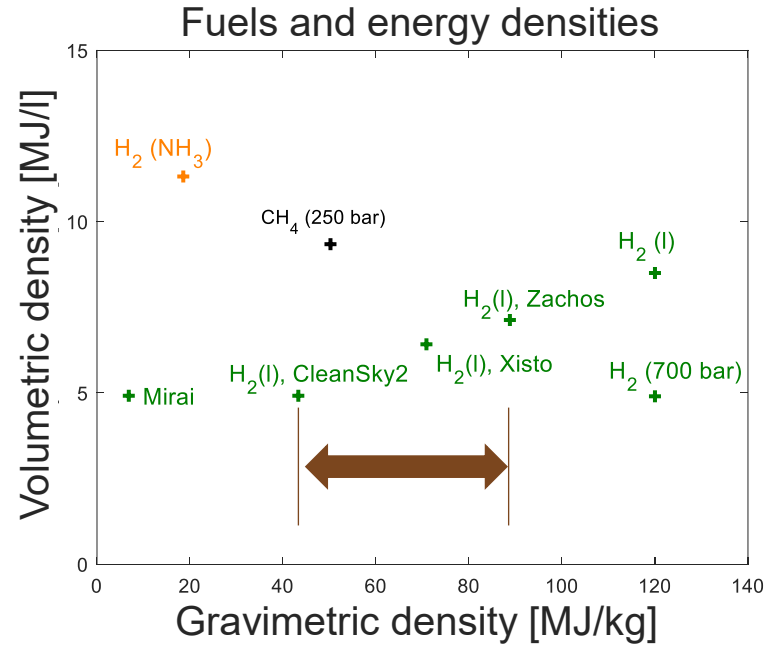
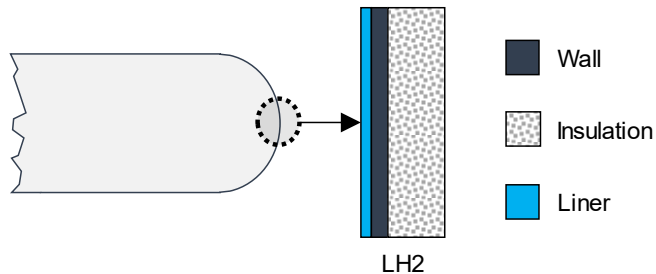


Installed cryo densities

- Clean Sky 2 estimates
 - Resulting in close to Jet A densities
 - Double wall vacuum tank
- Single wall, external isolation



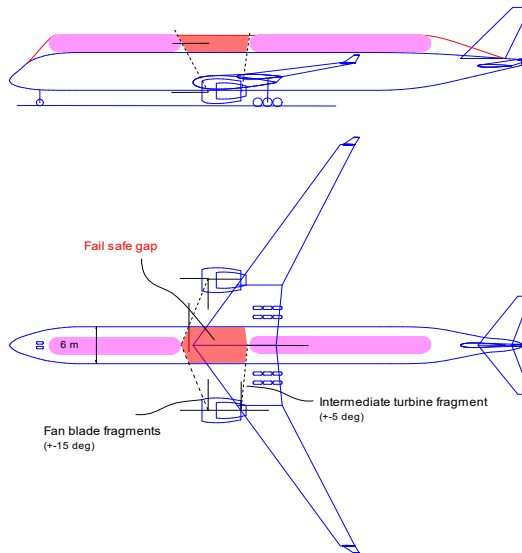
K. Dahal, S. Brynolf, C. Xisto, J. Hansson, M. Grahn, T. Grönstedt, M. Lehtveer, Techno-economic review of alternative fuels and propulsion systems for the aviation sector, Renewable and Sustainable Energy Reviews, Volume 151, 2021, 111564, ISSN 1364-0321,



- We can conclude that there is a large uncertainty in gravimetric density

Cryogenic hydrogen storage

- **ENABLEH2 (EU project)**
 - One project goal was to “revitalize interest in hydrogen for aviation”
- Insulated foam tanks are low TRL
- Double walled vacuum tanks are heavy (difficult with longer ranges)



 Baseline – low wings, tanks above fuselage	 1 – high wings, tanks above fuselage	 2 – low wings, external tanks below wings	 3 – high wings, external tanks below wings
 4 – low wings, external tanks above wings	 5 – external tanks joining box wings	 6 – conformal tanks either side of fuselage and below low wings	 7 – conformal tanks either side of fuselage and well below high wings
 8 – low wings, tank inside aft fuselage	 9 – high wings, tank inside aft fuselage	 10 – low wings, tanks in forward and aft fuselage	 11 – high wings, tanks in forward and aft fuselage
 12 – low wings, tank in centre of fuselage	 13 – high wings, tank in centre of fuselage	 14 – low wings, tank aft of double-bubble fuselage	 15 – high wings, tank aft of double-bubble fuselage
 16 – low wings, tanks at forward and aft ends of double-bubble fuselage	 17 – high wings, tanks at forward and aft ends of double-bubble fuselage	 18 – low wings, tank(s) in centre of double-bubble fuselage	 19 – high wings, tank(s) in centre of double-bubble fuselage
 20 – low wings, tanks aft and above double-deck fuselage	 21 – mid-height wings, tanks aft and above double-deck fuselage	 22 – low wings, tank(s) in centre of double-deck fuselage	 23 – mid-height wings, tank(s) in centre of double-deck fuselage
 24 – low wings, tanks at bottom of double-deck fuselage	 25 – mid-height wings, tanks at bottom of double-bubble fuselage	 26 – BWB with mid-height wings, internal under-floor tanks	 27 – BWB with mid-height wings, int. under-floor and external under-wing tanks
 28 – low wings, double fuselages, tanks inside aft fuselages	 29 – high wings, double fuselages, tanks inside aft fuselages	 30 – high wings, double fuselages, external tank on centreline	

Rompokos, P, Rolt A, Nalianda D, Isekveren A T, Senné C, Grönstedt T., Hamidreza A., Synergistic technology combinations for future commercial aircraft using liquid hydrogen”, Journal of Engineering for Gas Turbines and Power, Volume143, Issue, 7, 2021

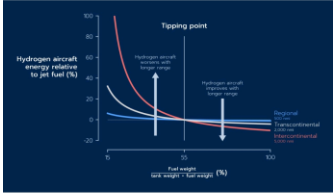


07:48 30%



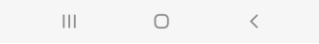
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Some say hydrogen-powered aircraft are only suitable for shorter flights, while others say they're better as the distance increases. This apparent contradiction stems from different assumptions on tank weight. In my review paper with Eytan Adler, we show that with light enough tanks, hydrogen aircraft could use less energy than current aircraft for all flight distances. You can read the full paper here: <https://lnkd.in/g/x7k5wkD>
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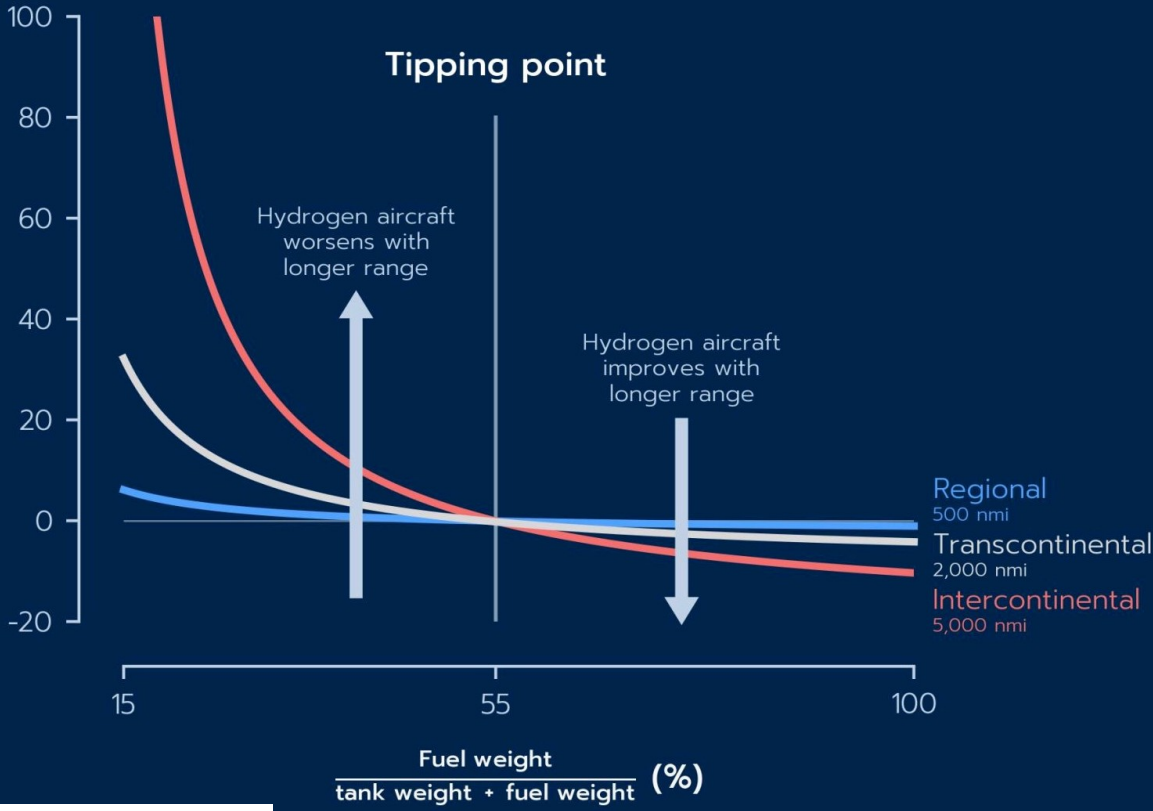


Well said ... Can I add ... Thanks for po

Skriv ner dina tankar här ... @ Lägg upp



Hydrogen aircraft energy relative to jet fuel (%)



Hydrogen-Powered Aircraft: Fundamental Concepts, Key Technologies, and Environmental Impacts

Eytan J. Adler* and Joaquim R. R. A. Martins
Department of Aerospace Engineering, University of Michigan, Ann Arbor, United States

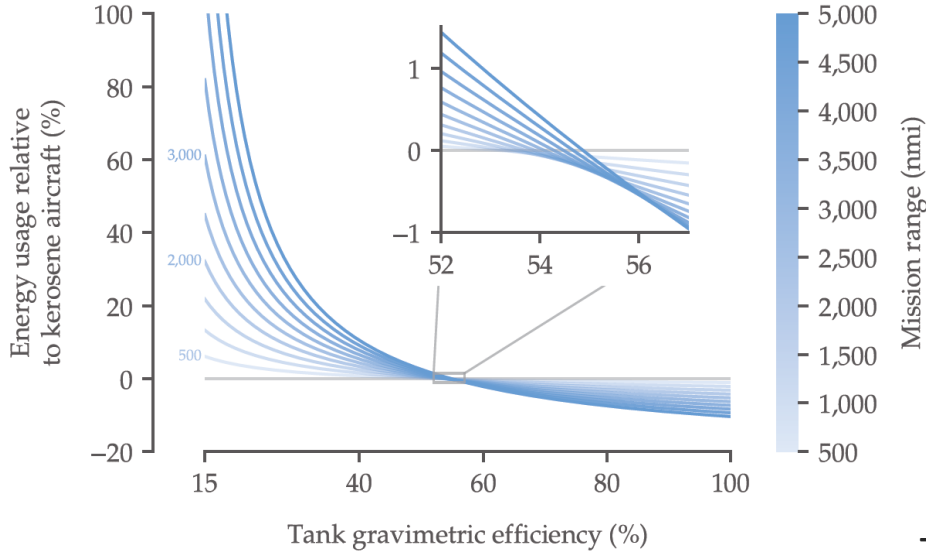
Version: December 11, 2022

Hydrogen-Powered Aircraft: Fundamental Concepts, Key Technologies, and Environmental Impacts

Eytan J. Adler* and Joaquim R. R. A. Martins

Department of Aerospace Engineering, University of Michigan, Ann Arbor, United States

Version: December 11, 2022



777-200LR

* Data is based on the Breguet range equation. It assumes a thrust-specific energy consumption based on the GE90 [48] and a cruise condition of Mach 0.8 at 35,000 ft. The lift-to-drag ratio is assumed to be 18. Tank weight is added to the base zero fuel weight. We found that the tipping point of 55% is insensitive to these parameter values.

For Martins data (in original paper) we repeat the chart. Where the gravimetric efficiency η is defined as:

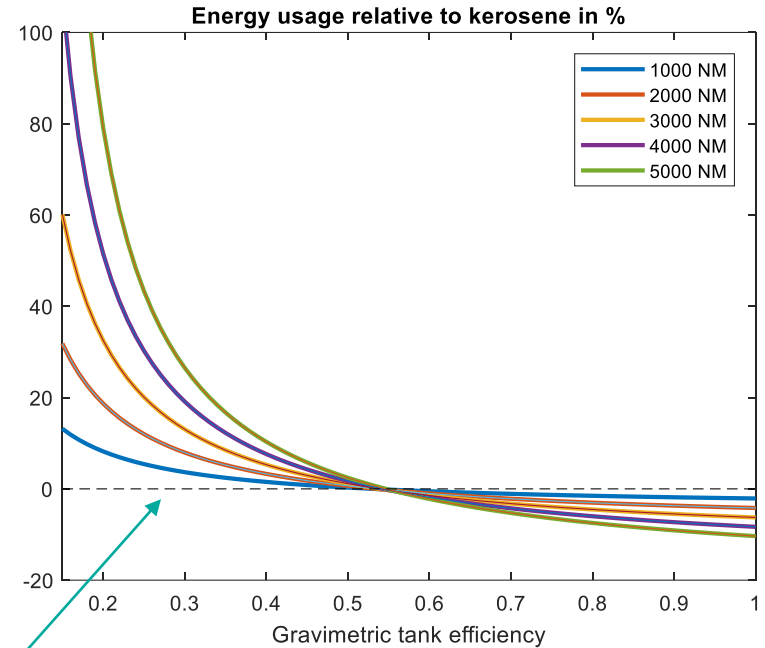
$$\eta = \frac{m_{fuel,H2}}{m_{fuel,H2} + m_{Tank,H2}}$$

Analytic solution for problem exist:

$$\alpha = \frac{\frac{Q_{H2}m_0 \left(1 - e^{-\frac{g \cdot R \cdot SFC_{H2}}{v \cdot \frac{L}{D}}}\right)}{Q_{JET-A} \cdot m_{fuel,JET-A}} + 1}{e^{-\frac{g \cdot R \cdot SFC_{H2}}{v \cdot \frac{L}{D}}} - 1}$$

Where the gravimetric efficiency relates to α as (easily derived from definition):

$$\eta = \frac{1}{1 + \alpha}$$

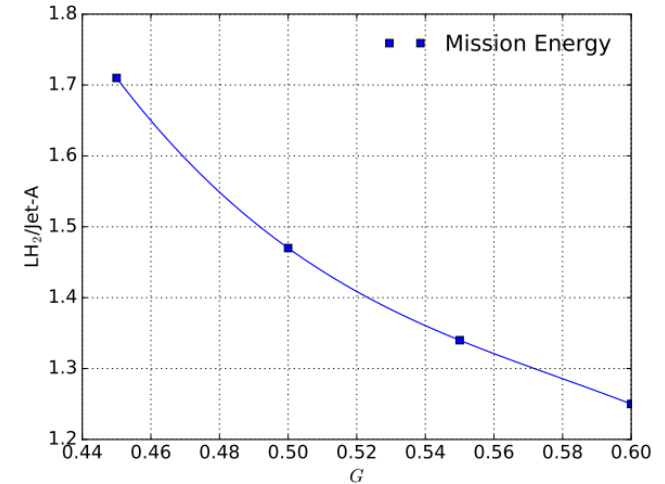
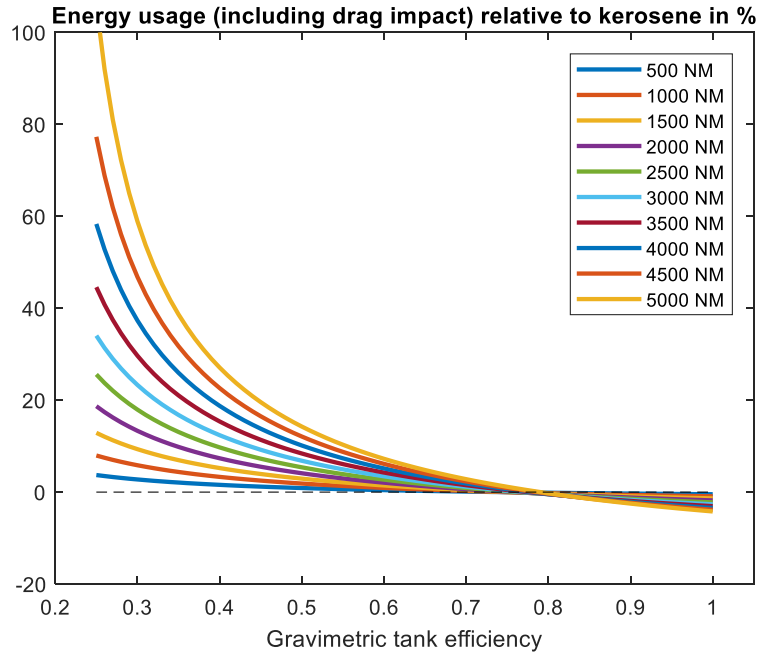


Nominal kerosene level

For the 5000 NM we get:

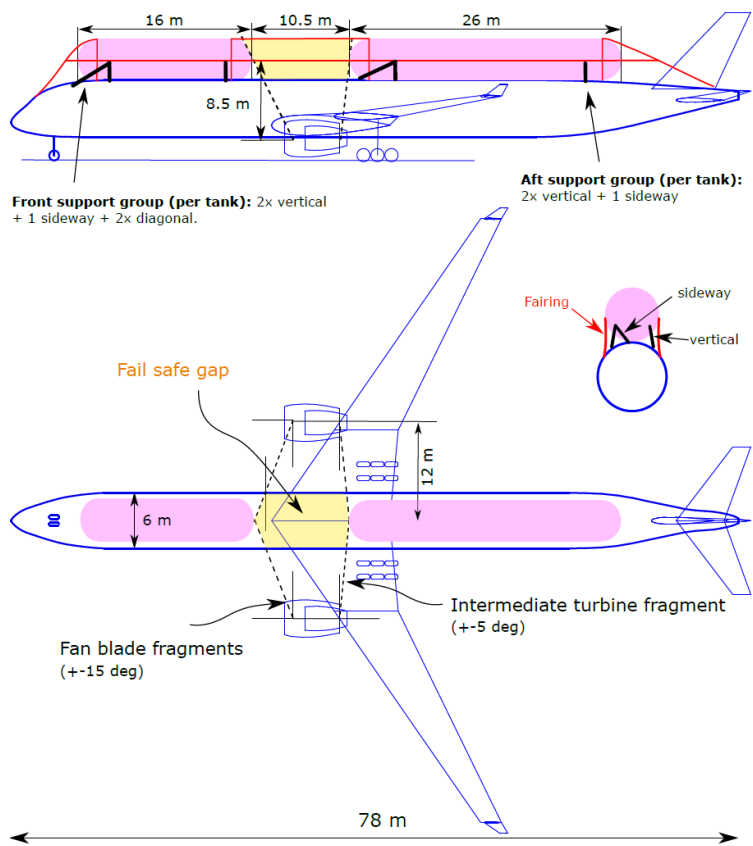
$$\alpha = 0.8289 \text{ and } \eta = 0.5468$$

- Now repeating with drag included (Raymer, Eq. 3.12)



- When added structural weight is considered NO cross over is found (always more energy need for H₂)

Xisto, C., Lundbladh, A., "Design and Performance of Liquid Hydrogen Fuelled Aircraft for Year 2050 EIS", ICAS, 2022



	Jet-A (2020)	Jet-A (2050)	LH2 (2050)	LH2 versus Jet- A (rel.)
MTOW (kg)	338,500	294,500	284,800	0.97
L/D	19.1	20.6	17.9	0.87
Wetted area fuselage (m ²)	1300	1300	1970	1.52
LH ₂ tank volume (m ³)	-	-	714	-
LH ₂ tank weight (kg) + structures and Fairing	-	-	26,500	-
Energy use (rel. to 2020)	Datum	-28%	-11%	-

*Gravimetric 65%
Foam insulated*

K. Dahal, S. Brynolf, C. Xisto, J. Hansson, M. Grahn, T. Grönstedt, M. Lehtveer,

Techno-economic review of alternative fuels and propulsion systems for the aviation sector, Renewable and Sustainable Energy Reviews, Volume 151, 2021



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